## Ashworth Engineering

Committed to on-time delivery of defect-free products and services, fit for use, exactly as promised, every time.

## PRODUCT TECHNICAL BULLETIN

## REDUCED RADIUS OMNI-GRID ${ }^{\text {® }}$

Turn Curve belting consisting of assembly of links and rods capable of accommodating turns in a conveyor system. Mesh overlays are available to give greater product support.

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## DEFINING CHARACTERISTICS

Inside Turning Radius: $1.6 \times$ Belt Width
Longitudinal Pitch: 1.08 inches [ 27.4 mm ]
Turn Capability: Capable of turning either right or left
Standard Belt Widths: 6 inches [ 152 mm ] through 40 inches [ 1016 mm ]
Maximum Allowable Tension: 150 lbs [667 N] entering and exiting a turn, 300 lbs . in straight run.
Conveying Surface: Belt width - 2.6 inches [ 66 mm ] less than nominal width
Method of Drive: Sprocket driven on both links
Basic Construction:

- Stainless Steel Materials
- 6 ga ( 0.192 inch [4.8 mm]) Connector Rod
- Wear Resistant ${ }^{\circledR}$ Links
- Heavy Duty Collapsing Links, Outside Edge
- Heavy Duty Reduced Radius Links, Inside Edge
- Omni-Tough® Mesh for Overlay


## BELT SPECIFICATIONS

| MESH OVERLAYS AVAILABLE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Omni-Tough ${ }^{\circledR}$ Wire: (Standard overlay for this product.) |  |  |  |  |
| Overlay Type | Mesh Designation | Minimum Belt Width in [mm] | Maximum <br> Belt Width in [mm] | $\begin{aligned} & \text { MESH OVERLAY: } \\ & \hline \text { Designation: } \end{aligned}$ |
| BALANCED WEAVE | *B12-12-16 ${ }^{\text {H }}$ | 12 [305] | 40 [1016] | First Digit: B = Balanced Weave; $\mathrm{U}=$ Unilateral Weave <br> X: First Number: No. of Loops per Foot of Width <br> Y: Second Number(s): No. of Spirals per Foot of Length (12 for 1in. pitch) |
|  | *B18-12-16 ${ }^{\text {H }}$ | 12 [305] | 40 [1016] |  |
|  | *B18-12-16 | 12 [305] | 40 [1016] |  |
|  | *B18-12-17 | 12 [305] | 40 [1016] |  |
|  | B24-12-16 | 6 [152] | 40 [1016] | Z: Third Number: Wire Gauge |
|  | B24-12-17 | 6 [152] | 40 [1016] | B30-12-17 |
|  | B30-12-16 | 6 [152] | 40 [1016] | U42-12-16 |
|  | B30-12-17 | 6 [152] | 40 [1016] |  |
|  | B36-12-16 | 6 [152] | 40 [1016] | Sizes: 14 through 18 ga. ( $.080 \mathrm{in} .[2.0 \mathrm{~mm}$ ]) through . 048 |
|  | B36-12-17 | 6 [152] | 40 [1016] | in. [1.2 mm] diameter) Material: annealed or high tensile |
|  | B42-12-16 | 6 [152] | 40 [1016] | spring wire (Omni-Tough ${ }^{\text {® }}$ ) |
|  | B42-12-17 | 6 [152] | 40 [1016] |  |
|  | B48-12-16 ${ }^{\text {H }}$ | 6 [152] | 40 [1016] |  |
|  | B48-12-17 ${ }^{\text {H }}$ | 6 [152] | 40 [1016] |  |
|  | U36-12-16 | 6 [152] | 40 [1016] |  |
| UNILATERAL WEAVE | U36-12-17 | 6 [152] | 40 [1016] | Inside Edge |
| - | U42-12-17 | 6 [152] | 40 [1016] |  |
|  | U48-12-17 | 6 [152] | 40 [1016] | - |
|  |  |  |  | REDUCED RADIUS OMNI-GRID ${ }^{\text {® }}$ |


| MESH OVERLAYS AVAILABLE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Omni-Tough ${ }^{\circledR}$ Wire: (Standard overlay for this product.) |  |  |  |  |
| Annealed Wire |  |  |  |  |
| BALANCED WEAVE | *B18-12-14 | 12 [305] | 40 [1016] |  |
|  | *B18-12-18 | 12 [305] | 40 [1016] |  |
|  | B30-12-18 | 6 [152] | 40 [1016] |  |
|  | B36-12-14 | 6 [152] | 40 [1016] |  |
|  | B48-12-14 | 6 [152] | 40 [1016] |  |
|  | B48-12-18 | 6 [152] | 40 [1016] |  |
|  | B60-12-18 | 6 [152] | 40 [1016] |  |
|  |  |  |  |  |

## NOTES:

*Minimum width of 12 inches ( 304.8 mm ), overall.
${ }^{\mathrm{H}}$ Available in half hard wire only not Omni-Tough.

- The first set of numbers in the mesh designation indicates the number of spiral loops per foot of width.
- The second number specifies the number of pitches per linear foot.
- The last number is the wire gauge of the mesh.


## BELT WEIGHT

| Mesh <br> Lateral Count | $\begin{gathered} 18 \text { ga . } 0475 \mathrm{in} . \\ {[1.2 \mathrm{~mm}]} \\ \hline \end{gathered}$ |  | $\begin{gathered} 17 \mathrm{ga} .054 \mathrm{in} . \\ {[1.4 \mathrm{~mm}]} \end{gathered}$ |  | $\begin{gathered} 16 \mathrm{ga.} .0625 \mathrm{in} . \\ {[1.6 \mathrm{~mm}]} \end{gathered}$ |  | $\begin{gathered} 14 \mathrm{ga} .080 \mathrm{in} . \\ {[2.0 \mathrm{~mm}]} \\ \hline \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | lbs/ft ${ }^{\text {² }}$ | $\mathrm{kgs} / \mathrm{m}^{2}$ | lbs/ft ${ }^{2}$ | $\mathrm{kgs} / \mathrm{m}^{2}$ | lbs/ft ${ }^{\text {2 }}$ | $\mathrm{kgs} / \mathrm{m}^{2}$ | lbs/ft ${ }^{2}$ | $\mathrm{kgs} / \mathrm{m}^{2}$ |
| 12 | -- | -- | -- | -- | . 38 | 1.9 | -- | -- |
| 18 | . 31 | 1.5 | . 42 | 2.1 | . 55 | 2.7 | . 94 | 4.6 |
| 24 | -- | -- | . 56 | 2.7 | . 74 | 3.6 | -- | -- |
| 30 | . 51 | 2.5 | . 68 | 3.3 | . 93 | 4.5 | -- | -- |
| 36 | -- | -- | . 82 | 4.0 | 1.08 | 5.3 | 1.84 | 9.0 |
| 42 | -- | -- | . 95 | 4.6 | 1.26 | 6.2 | -- | -- |
| 48 | . 82 | 4.0 | 1.08 | 5.3 | 1.44 | 7.0 | 2.44 | 11.9 |
| 60 | 1.02 | 5.0 | -- | -- | -- | -- | -- | -- |


|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BELT <br> WIDTH |  | TURN RADIUS |  | BELT BASE <br> WEIGHT |  |
| $\mathbf{\text { in. }}$ | $\boldsymbol{m m}$ | in. | $\boldsymbol{m m}$ | lbs/ft | $\boldsymbol{k g s} / \boldsymbol{m}$ |
| 6 | 152 | 9.6 | 244 | 1.37 | 2.04 |
| 8 | 203 | 12.8 | 325 | 1.56 | 2.32 |
| 10 | 254 | 16.0 | 406 | 1.74 | 2.60 |
| 12 | 305 | 19.2 | 488 | 1.93 | 2.88 |
| $\mathbf{1 4}$ | 356 | 22.4 | 569 | 2.12 | 3.15 |
| 16 | 406 | 25.6 | 650 | 2.30 | 3.43 |
| 18 | 457 | 28.8 | 732 | 2.49 | 3.71 |
| 20 | 508 | 32.0 | 813 | 2.68 | 3.99 |
| 22 | 559 | 35.2 | 894 | 2.86 | 4.27 |
| 24 | 610 | 38.4 | 975 | 3.05 | 4.54 |
| 26 | 660 | 41.6 | 1057 | 3.24 | 4.82 |
| 28 | 711 | 44.8 | 1138 | 3.42 | 5.10 |
| 30 | 762 | 48.0 | 1219 | 3.61 | 5.38 |
| 32 | 813 | 51.2 | 1301 | 3.79 | 5.65 |
| 34 | 864 | 54.4 | 1382 | 3.98 | 5.93 |
| 36 | 914 | 57.6 | 1463 | 4.17 | 6.21 |
| 38 | 965 | 60.8 | 1544 | 4.35 | 6.49 |
| 40 | 1016 | 64.0 | 1626 | 4.54 | 6.77 |

Consult out Product Engineers for approval of wider belt widths and concerns regarding belt tension or turn ratio.

## BELT OPTIONS

## DESCRIPTION

GUARD EDGE PLATE


## INTEGRAL GUARD EDGE



## PURPOSE

Plates assembled between links and mesh to prevent product from falling off belt. Guard edge plates are tack welded to links as needed to secure position.

## AVAILABILITY <br> Outside belt edge only.

Height Above Conveying Surface:
0.50 inch [ 12.7 mm ]
0.75 inch [ 19.1 mm ] 1.00 inch [25.4 mm]

Edge of link raised to prevent product from falling off of belt. Integral guard edge links offer improved cleanup and sanitation over guard edge plates. Outside belt edge only.

Height Above Conveying Surface
0.75 inch [19.1 mm]
1.00 inch [25.4 mm] 1.50 inches [ 38.1 mm ] 2.00 inches [ 50.8 mm ]

Raised edge may be on the inside or outside edge of the link.

## OMNI-TOUGH ${ }^{\text {® }}$

- Provides a flatter mesh surface with a high resilience to impact.
- Available for most belt widths in most mesh configurations. Available in 16 and 17 ga . only.


## VARIABLE LOOP COUNT

(Patent No. 6,129,205)

- When belt collapses on inside edge to accommodate a turn, product support is maximized and wire overlay does not overlap.
- Mesh count is more open on the inside belt edge and progressively gets tighter across the width of the belt.
- Available in Omni-Tough ${ }^{\circledR}$ only
- Turn direction must be specified.
- Mesh designated as follows: B42/24-12-17 where belt has an inside mesh of 24 progressing to 42 spirals/foot.


## SPECIAL SPIRALS

- Available in Omni-Tough ${ }^{\circledR}$ only
- One or more spirals on conveying surface is raised
- Used as guard edges, lane dividers and flights
- Maximum height equal to belt pitch
- Available Options: height, spacing, location, shape and number of lanes in belt.


## SPROCKETS



Right Triangle


Isosceles Triangle

OUISIDEEDGE


Standard UHMW sprockets for 1.08 inch pitch belts.

| No. of Teeth | Overall Diameter |  | Pitch Diameter |  | Flange Diameter |  | Flange Width |  | Hub Width |  | HubDiameter \& Type |  | Bore |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | inch | mm | inch | mm | inch | mm | inch | mm | inch | mm | inch | mm | inch | mm | inch | Mm |
| 9 | 3.53 | 89.7 | 3.16 | 80.2 | -- | -- | -- | -- | 2.00 | 51.0 | 2.53 | 64.3 | . 813 | 20.6 | 1.44 | 36.5 |
| 13 | 4.90 | 124.5 | 4.53 | 115.1 | -- | -- | -- | -- | 2.00 | 50.8 | 3.90 | 99.1 | 1.00 | 25.4 | 2.19 | 55.6 |
| 18 | 6.65 | 168.9 | 6.24 | 158.5 | -- | -- | -- | -- | 2.00 | 50.8 | 5.65 | 143.5 | 1.00 | 25.4 | 3.75 | 95.3 |
| 23 | 8.39 | 213.0 | 7.96 | 202.2 | -- | -- | -- | -- | 2.00 | 50.8 | 7.39 | 187.6 | 1.00 | 25.4 | 4.00 | 101.6 |
| 31 | 11.16 | 283.5 | 10.72 | 272.3 | -- | -- | -- | -- | 2.00 | 50.8 | 101.6 | 258.1 | 1.00 | 25.4 | 7.13 | 183.0 |
| 37 | 13.24 | 336.2 | 12.73 | 323.5 | -- | -- | -- | -- | 2.00 | 50.8 | 12.24 | 310.8 | 1.00 | 25.4 | 8.94 | 277.0 |

Steel sprockets for 1.08 inch pitch belts.

| No. of Teeth | Overall <br> Diameter |  | Pitch <br> Diameter |  | Flange Diameter |  | Flange Width |  | Hub Width |  | HubDiameter \& Type |  | Bore |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | inch | mm | inch | mm | inch | mm | inch | mm | inch | mm | inch | mm | inch | mm | inch | Mm |
| 13 | 4.80 | 124.5 | 4.53 | 115.1 | -- | -- | -- | -- | 2.00 | 51.0 | 3.90 | 99.1 | 1.00 | 25.4 | 2.19 | 55.6 |

## NOTES:

- UHMWPE material type components have a $150^{\circ} \mathrm{F}\left[66^{\circ} \mathrm{C}\right]$ maximum operating temperature.
- Maximum bore sizes listed for UHMWPE material is based on $1 / 2$ inch [12.7 mm ] of material above keyway.


## SUPPORT

Supports are required on a maximum of 6 inches apart on load side and 12 inches maximum on return side. Rollers may also be used.
NOTE: For heavier load applications, additional support rollers may be required.

## WEARSTRIP PLACEMENT

## 18 TOOTH UHMW PE SPROCKET



$$
A=1 / 2 X P D-0.25 \text { inch }[6.4 \mathrm{~mm}]
$$

- This is only a guideline; it does not take into account the influence of speed.
- At speeds above $75 \mathrm{ft} / \mathrm{min}$ [ $23 \mathrm{~m} / \mathrm{min}$ ] Ashworth recommends increasing the distance A and shortening the wear strips as much as one belt pitch in length. (Nominal Belt Pitch $=1.08$ inches [27.4 mm]])


## ENGINEERING CALCULATIONS

| Coefficient of Friction | Type of Support Structure |
| :---: | :---: |
| .15 | Nylon-12 under overlay (unlubricated) |
| .15 | Acetal under overlay (unlubricated) |
| .10 | Acetal under overlay (lubricated) |
| .15 | Steel support rails (lubricated) |
| .20 | Steel support rails (unlubricated) |
| .20 | UHMW under links (unlubricated) |

## TURN RATIO

$$
\mathrm{TR}=\mathrm{ITR} \div \mathrm{BW}
$$

where $\quad$ ITR $=$ Inside Turn Radius BW = Belt Width

Turn Ratio is dimensionless. Inside Turn Radius and Belt Width must both be in same unit of measurement, either both in units of inches or both in units of millimeters.

| Belt Type | Tension Link | Turn Radius to Tension Link |
| :--- | :--- | :--- |
| 1 inch Pitch Omni-Grid | Outside Link | ITR + Belt Width |

## BELT WEIGHT



Belt Weight $=($ Weight of Base Belt $)+($ Weight of Mesh Overlay $)$

## STEPS OF CALCULATION:

- Determine weight of base belt in lbs./feet or $\mathrm{kgs} /$ meter.
- Calculate conveying surface and convert to units of feet or meters.
- Use the conveying surface and mesh type to determine weight of mesh in lbs./feet or $\mathrm{kgs} /$ meter.
- Add weight of base belt to weight of mesh overlay, lbs./feet or kgs/meter
- Multiply calculated value by belt length (feet or meters) for total belt weight in units of lbs. or kgs.


## BELT TENSION

Estimated belt tension in a straight run:
$\mathrm{T}=\left(\mathrm{wLfr}+\mathrm{WLf}_{1}+\mathrm{WH}\right) \times \mathrm{C}$
Metric Units:
Where $\quad \mathrm{T}=$ Belt Tension (lbs. force/linear ft of belt width)
W = Belt Weight (lbs./linear ft.)
$\mathrm{W}=$ Total Weight $=$ Belt Weight + Product Weight (lbs./linear ft)
$\mathrm{L}=$ Conveyor Length or center to center of terminals (feet)
[newtons]
[kg/linear meter]
$\mathrm{H}=$ Rise of incline Conveyor $\{+$ if incline, - if decline\} (feet)
[kg/linear meter]
[meters]
$\mathrm{f}_{1}=$ Coefficient of Friction between belt and belt supports, load side
[meters]
$f_{r}=$ Coefficient of Friction between belt and belt supports, return side
dimensionless
C = Force Conversion Factor
Imperial: 1.0
Metric: 9.8

## SYSTEM REOUIREMENTS



POSSIBLE SYSTEM TENSION INDICATORS

1. DRIVE MOTOR AMP. READING
2. TAKE-UP ROLL POSITION 3. DIRECT MEASUREMENT

## LUBRICATION

Lubrication with silicone may be necessary on the belt support rails in some cases. The best method of application is by brush, fed from a drip reservoir, brushed onto the bottom in the return so that the belt applies the lubricant to the rails on the load side. Apply lubricant until the take-up rises or the drive amp reading drops to set values determined by testing.
Typically a customer uses 8 ounces per week on a system employing 1500 feet of belt in a 24 hour a day operation. As you can see, this is a very small amount of oil and dripping should not be a problem.

## SWING WIDE

The belt tends to "swing wide" as it exits the spiral cage or turn curve, following a path that is offset but parallel to the normal tangent line to the cage. This phenomena itself does no damage, but often the belt edge contacts framework that does not leave sufficient clearance for this to occur. The usual reaction of the builders or users is to restrict the path of the belt from swinging wide, typically by use of rollers or shoe guides.
Restraining the belt path can have several adverse effects on belt life:

- The belt can wear through a shoe guide, allowing the edge to snag. This will eventually cause an increase in belt tension and damage the belt edge.
- Outside edge restraints can push individual rods inward. The rods can be held in this inward position by belt tension. There is then a potential for the projecting rods to catch on the vertical cage bar capping, causing damage to the belt, damage to the cage bar capping, and high belt tension.
If the belt is pushed into a straight tangent path, the tension carried in the outside edge of the belt is shifted to the inside edge of the belt, resulting in a pronounced tendency for one edge of the belt to lead the other.

Reference: Product Technical Bulletin "Conveyor Design Guidelines".


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